



AC Electric Fields Drive Steady Flows in Flames

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Manipulating flames at a distance with AC electric fields

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Abstract. We show that time-oscillating electric fields applied to plasmas present in flames create steady flows of gas. Ions generated within the flame move in the field and migrate a distance δ before recombining; the net flow of ions away from the flame creates a time-averaged force that drives the steady flows observed experimentally. A quantitative model describes the response of the flame and reveals how δ decreases as the frequency of the applied field increases. Interestingly, above a critical frequency, AC fields can be used to manipulate flames at a distance without the need for proximal electrodes.

The most familiar description of a flame is “a local region of high temperature generated by rapid, exothermic chemical reactions”. A flame is, however, also a plasma. In particular, the combustion of hydrocarbon fuels generates sufficient densities of charged species that even small flames (the flame of a humble candle) can be considered as chemically driven, nonequilibrium plasmas [1]. As such, flames interact with external electric fields, which can be used to monitor [2], manipulate [3, 4], and enhance [5, 6] the processes that make up “combustion” through a variety of physical and chemical mechanisms. Sufficiently strong electric fields ($>10^6$ V/m at atmospheric pressure) influence the chemistry of combustion by accelerating electrons to energies capable of exciting, dissociating, or ionizing neutral species upon impact [6]. Even fields that are too weak to influence combustion directly can cause

significant hydrodynamic flows [1] – so called electric or ionic winds [7] – through the collisional transfer of momentum from accelerated charged species to the neutral gas [8, 9].

Previous efforts to manipulate flame plasmas with electric winds have relied almost exclusively on static (DC) fields [1] to induce steady currents of charged species that drive steady gas flows (although see [4, 10, 11]). Despite promising demonstrations (e.g., enhancing flame stability [5], manipulating heat transfer [3], reducing pollutant emissions [12]), the magnitude of these effects – and their applicability – is strictly limited by ionic screening, which requires direct contact of the electrodes and the flame to maximize the ionic currents and gas velocities [8].

Here, we report that time-oscillatory (AC) electric fields also induce *steady* electric winds in flame plasmas with gas velocities exceeding those due to static fields of comparable magnitude. Furthermore, unlike static fields, the electric force due to AC fields is localized near the surface of the flame. Consequently, the AC response depends only on the local field at the surface of the flame – not on the position of the electrodes used to generate the field. These results suggest that oscillating electric fields can be used to manipulate and control combustion processes at a distance.

To characterize and explain these effects, we investigated a simple experimental system comprising a laminar methane-air flame positioned between two parallel-plate electrodes. We quantify both the electric and hydrodynamic response of the flame as a function of frequency and magnitude of the applied field. A theoretical model shows how steady gas flows emerge from the time-averaged electrical force due to the field-induced motion of ions generated within the flame and by their disappearance by recombination. Our predictions of both the flow velocity and the electric response agree quantitatively with the experimental results.

Experimental. A small methane flame was positioned symmetrically between two parallel aluminum electrodes (20 cm × 20 cm), separated by a distance $L = 10$ cm (Fig. 1a). The burner was a thermally and electrically insulating cylindrical tube (alumina composite, i.d. 6.4 mm, o.d. 9.5 mm) through which flowed a mixture of methane, oxygen, and nitrogen (molar composition, $\text{CH}_4:\text{O}_2:\text{N}_2 = 0.15:0.17:0.68$; flow rate = 500 sccm; equivalence ratio, $\phi = 1.75$, with air as oxidizer). When needed, the nitrogen stream was doped with a fine mist (1–10 μm droplets, created by an ultrasonicator) of 1M aqueous NaOH to increase the density of ions within the flame [13, 14]. To mitigate external air flows, we enclosed the

flame and the electrodes in a glass box (30×30×30 cm) with a central, triangular opening (~20 cm) in its top to vent combustion products.

A high-voltage amplifier (Trek 40/15) applied sinusoidal, time-varying electric fields to the flame. AC fields caused the transient redistribution of charged species generated within the flame and resulted in the formation of two gas jets directed symmetrically outwards towards the two electrodes (Fig. 1b). To characterize the response of the flame, we measured two quantities (i) the electric current I through the circuit illustrated in Figure 1a using an analog preamplifier (DL Instruments 1211) interfaced with a data acquisition system (NI-9223), and (ii) the velocity of the field-induced gas flows using high-speed schlieren velocimetry [15, 16].

Static Fields. As previously reported [1, 8], the application of a static field to a methane flame creates an electric wind (Fig. 2a shows $E_o = 280$ kV/m). Charge carriers generated within the flame migrate to the respective electrodes, with positive [17] and negative [18] charges moving with and against the direction of the field. The accumulation of charge on both sides of the flame results in an electric force density $f = \rho E$ (ρ is the charge density, E is the local electric field) that drives two jets of gas in opposite directions. To contrast this DC response with the AC effect described below, we briefly quantify the effect of static electric fields in the experimental set-up used here.

The electric force density f driving the flow is directly proportional to the electric current I , which can be measured directly (Fig. 2b); this proportionality holds because the electric force is approximately $f \approx q_{\pm} n_{\pm} E$ while the current density is $j \approx q_{\pm} K_{\pm} n_{\pm} E \sim I$, where q_{\pm} , n_{\pm} , and K_{\pm} are the charge, number density (ions/volume), and mobility (drift velocity/field strength) of the charge carriers. For the methane flame without NaOH dopant, the current increases quadratically with the field before saturating at a constant value. At low fields, the accumulation of charge on both sides of the flame acts to screen the field in the region of the flame and limits the current. Within the space-charge regions, the ion density is proportional to the applied field $n_{\pm} \sim E_o$, and the current scales as $j \sim E_o^2$ [1, 8, 16]. For sufficiently strong fields, the current is instead limited by the rate of ionization within the flame – that is, all charged species generated by combustion are removed by the field via the electrodes. By doping the flame with additional ions, the transition from the space-charge-limited regime to the reaction-limited regime can be shifted to larger fields (Fig. 2b).

In the space-charge-limited regime, the velocities of the gas jets increase linearly with the magnitude of the applied field (Fig. 2c) as explained by Bernoulli's principle [1]. Briefly, the pressure drop is proportional to the electric force $\Delta p \sim f$, which in turn is proportional to the current density $f \sim j$, such that $\Delta p \sim j \sim E_o^2$. The characteristic velocity is therefore $u = (\Delta p / 2\rho_f)^{1/2} = C E_o$, where ρ_f is the fluid density and C is a constant. Assuming $\Delta p \approx \varepsilon_o E_o^2$ (cf. below), these scaling arguments suggests $C \approx 3.9 \times 10^{-6} \text{ m}^2 \text{ V}^{-1} \text{ s}^{-1}$ – as compared to $C = 2.9 \times 10^{-6} \text{ m}^2 \text{ V}^{-1} \text{ s}^{-1}$ determined experimentally (Fig. 2c).

Oscillating Fields. Application of an AC field, $E(t) = \sqrt{2} E_o \cos(\omega t)$, to a doped flame creates an electric wind similar to that produced by a static field: two gas jets flow outwards from the flame towards the electrodes (Fig. 1b shows $\nu = \omega / 2\pi = 1 \text{ kHz}$ and $E_o = 100 \text{ kV/m}$). Because the applied field is symmetric, the jets are nearly identical in shape, and their velocity increases strongly with increasing field strength E_o and weakly with increasing frequency ν (Fig. 3a). At low frequencies, the gas velocity is well described by the DC relation from Figure 2c. At higher frequencies, the velocity increases by ca. 20% at the highest frequencies accessible by the amplifier ($\sim 1 \text{ kHz}$).

To characterize the electric response of the flame, we calculated the energy dissipation rate $\Phi = \langle I(t)V(t) \rangle$ due to the motion of charged species in and around the flame as a function of frequency and field strength (Fig. 3b), where $I(t)$ is the measured current, $V(t)$ is the applied voltage, and $\langle \rangle$ denotes a time average. In the absence of the flame, the dissipation rate is negligible, as expected for an ideal capacitor; the measured dissipation rate thus characterizes the electric response of the flame itself [16].

At low frequencies, Φ approaches a constant value corresponding to the oscillation average of the DC current-voltage relationship $I_{dc}(V)$ in Figure 2b – that is, $\Phi \approx \langle I_{dc}(V(t)) \cdot V(t) \rangle$. Using the quadratic fit $I_{dc} = D V^2$ from Figure 2b with $D = 1.1 \times 10^{-14} \text{ A V}^{-2}$, the low-frequency dissipation rate is approximately $\Phi \approx (8\sqrt{2}D / 3\pi) V_o^3$ where $V_o = L E_o$ (e.g., for $E_o = 200 \text{ kV/m}$, $\Phi \approx 0.11 \text{ W}$ in quantitative agreement with experiment; cf. Fig. 3b). Above a critical frequency (dashed curve in Fig. 3b), the dissipation rate increases by a factor of ~ 5 at the highest frequencies ($\sim 1 \text{ kHz}$); this increase suggests a transition in the structure of the flame plasma due to the AC field.

Discussion. Electrohydrodynamic flows are driven by an electric body force of the form $f = \rho E$, which enters into the Navier-Stokes equations governing fluid motion. For simplicity, we consider the one-dimensional geometry illustrated in Figure 4a. Gauss's law implies that the electric force can be expressed

as $f(x,t) = \varepsilon_o \partial E^2(x,t) / \partial x$. Averaging in time over one period of oscillation gives $\langle f \rangle = \varepsilon_o d \langle E^2 \rangle / dx$. For the experimental conditions, the field inside the flame is negligible, $\langle E^2 \rangle \approx 0$, due to screening by mobile charged species. Far from the flame, the average field strength approaches that of the applied field, $\langle E^2 \rangle \approx E_o^2$. The transition of $\langle E^2 \rangle$ from 0 to E_o^2 occurs across some region of size δ within which the electric force is localized (*cf.* below). Furthermore, the force is directed outwards from the flame in either direction (*i.e.*, from regions of weak field to regions of strong field in qualitative agreement with the gas jets observed in experiment).

To estimate the gas velocities induced by the steady electric force, we define a characteristic pressure drop $\Delta p \approx \varepsilon_o E_o^2$ by integrating the force from inside the flame to some point far from the flame. Bernoulli's principle then implies a characteristic velocity of $u \approx (2\varepsilon_o / \rho_f)^{1/2} E_o$ – identical to that derived for static fields.

To determine the length scale δ over which the force is distributed, we must consider the details of the charge transport in and around the flame. We consider the following model describing the production and consumption of ions within the flame and their transient migration in the field [16].

$$\frac{\partial n_{\pm}}{\partial t} + \frac{\partial}{\partial x} (\pm K n_{\pm} E) = k_i g(x) - k_r n_+ n_- \quad (1)$$

$$\frac{\partial E}{\partial x} = \frac{e}{\varepsilon_o} (n_+ - n_-) \quad \text{where} \quad \int_0^L E dx = \sqrt{2} L E_o \cos(\omega t) \quad (2)$$

Here, the charge carriers are assumed to be monovalent ions with equal mobilities $\pm K \sim 10^{-4} \text{ m}^2 \text{ V}^{-1} \text{ s}^{-1}$ [19]; the flame is represented by a localized region of ionization $g(x)$ with a characteristic thickness $a \sim 10^{-4} \text{ m}$ (Fig. 4a) and magnitude $k_i \sim 10^{20} \text{ ions m}^{-3} \text{ s}^{-1}$ [20]. Ions are consumed through a second-order recombination process with rate constant $k_r \sim 10^{-13} \text{ ions}^{-1} \text{ m}^3 \text{ s}^{-1}$ [20] or by perfectly absorbing electrodes at the system boundaries. Remarkably, this simple model predicts the average dissipation rate as a function of both frequency and field strength in quantitative agreement with experiments (Fig. 3b solid curves).

Further analysis [16] reveals the length scale over which ions are redistributed by the field: $\delta \sim K E_o / \kappa \omega$ where $\kappa = (\varepsilon_o k_r / e K)^{1/2} \sim 0.3$ is a dimensionless parameter characterizing the relative rates of ion recombination ($k_r n_o$ where $n_o = (k_i / k_r)^{1/2}$) and ion screening ($e K n_o / \varepsilon_o$). Briefly, we rewrite equations (1)

in terms of the total ion density $n_s = n_+ + n_-$ and the charge density $n_d = n_+ - n_-$, maintaining only the dominant terms.

$$\frac{\partial n_s}{\partial t} + \frac{\partial}{\partial x}(Kn_d E) = k_i g(x) - \frac{1}{4}k_r(n_s^2 - n_d^2) \quad (3)$$

$$\frac{\partial n_d}{\partial t} + \frac{\partial}{\partial x}(Kn_s E) = 0 \quad (4)$$

Approximating $\partial/\partial t$ as ω , $\partial/\partial x$ as δ^{-1} , and field strength by E_o , equations (2) – (4) yield the characteristic length scale $\delta \sim KE_o/\kappa\omega$, ion density $n_s \sim \varepsilon_o\omega/eK$, and charge density $n_d \sim \kappa\varepsilon_o\omega/eK$. Examining the magnitude of the neglected terms, this dominant balance governs charge transport *outside* of the flame (where $g(x) \sim 0$) provided $\delta \ll L$ and $\kappa \ll 1$.

From a *microscopic* perspective, ions generated within the reaction zone migrate a distance δ under the influence of the field before recombining. The migration of a single ion creates an impulse (force \times time) of order $\delta e/K$, which is transferred to the neutral gas through molecular collisions. Multiplying this impulse by the net flux of ions leaving the ionization region yields the pressure difference Δp driving the flow. Using the scaling arguments above, the ion flux $Kn_d E$ may be approximated as $\omega\kappa\varepsilon_o E_o/e$ such that $\Delta p \sim \varepsilon_o E_o^2$ in agreement with the *macroscopic* derivation above.

When δ is larger than L ($\omega \ll KE_o/\kappa L$), ions are consumed at the absorbing electrodes, and the dissipation rate is identical to that observed for static fields averaged over one period of oscillation – namely, $\Phi_{low} \approx [6\sqrt{2}L^3/\pi(L-b)^3]A_f\varepsilon_oKE_o^3$, where A_f is the characteristic area of the flame (needed to convert the results of the 1D model into 3D), and b is the width of the flame (see Fig. 4a). Above a critical frequency (*i.e.*, when $\delta \ll L$ or $\omega \gg KE_o/\kappa L$; dashed curve in Fig. 3b), ions are instead consumed via chemical recombination processes within a thin region surrounding the flame (*e.g.*, $\delta \sim 5$ mm for $\nu = 1$ kHz and $E_o = 100$ kV/m). In this limit, the average dissipation rate increases to $\Phi_{high} = (4\sqrt{2}/\kappa)A_f\varepsilon_oKE_o^3$ and no longer depends on the position of the electrodes (*i.e.*, on L).

Consequently and in contrast to flows driven by static fields, AC electric winds do not require electrical contact between the flame and the surrounding electrodes. This independence is illustrated in Figure 4b, in which the electrodes have been covered with an electrically insulating material. Upon application of a

static field, charge rapidly accumulates on the insulating surfaces, screens the applied field, and prevents the formation of electric winds. The response to an oscillating field is unchanged.

At even higher frequencies – namely, for $\omega > eKn_o / \epsilon_o$ – the field varies faster than the time required for ions to redistribute and screen the field within the flame. No flows are expected at such frequencies. For the flame plasmas described here, $n_o \sim 10^{16} - 10^{17}$ ions m^{-3} [16], and electric winds are expected only for frequencies $\nu < 10\text{--}100$ kHz.

Conclusions. Oscillating electric fields interact with the plasmas generated by combustion of methane to create steady flows of gas. In contrast to electrical forces due to static fields, the forces induced by AC fields act directly at the surface of the flame, and do not depend on the position of the electrodes. Importantly, these results provide a basis for the “electrode free” manipulation and control of combustion processes – *e.g.*, by electromagnetic waves. Beyond the symmetric flows detailed here, it should also be possible to achieve directional flows by varying the geometry of the applied field.

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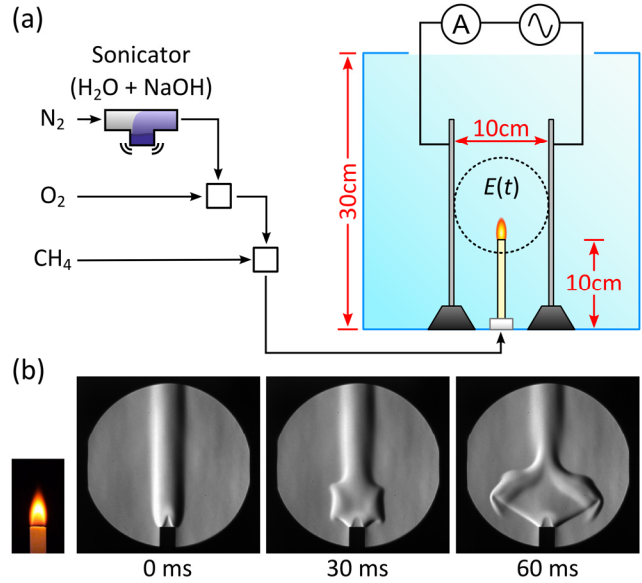


Figure 1. (color online) **(a)** Schematic illustration of the experimental set-up; the cubic combustion chamber is drawn to scale. The dotted circle illustrates the field of view for the schlieren images below. **(b)** Schlieren images of a premixed, NaOH-doped methane flame following the application of an oscillating electric field of magnitude $100 \text{ kV}_{\text{RMS}}/\text{m}$ at 1 kHz . The images are taken at intervals of 30 ms following the application of the field.

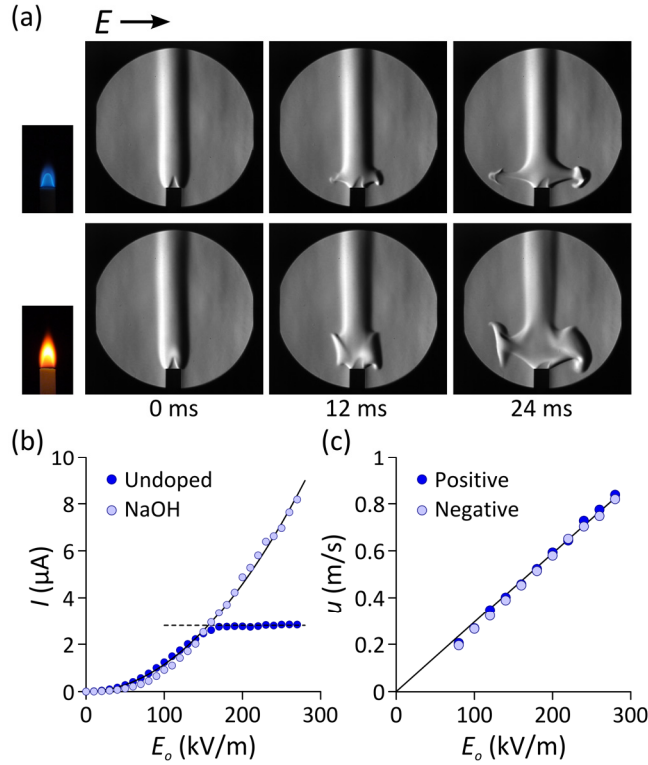


Figure 2. (color online) *Static fields.* **(a)** Schlieren images of a premixed methane flame without (*top*) and with (*bottom*) NaOH dopant directly after the application of a static electric field of 280 kV/m. The images are taken at regular intervals of 12 ms. **(b)** Electric current as a function of the applied field strength for a premixed methane flame with (\circ) and without (\bullet) ion doping. The solid and dashed lines illustrate the space charge limited and reaction limited responses, respectively; the fit used for the space charge response is $I = (1.1 \times 10^{-16} \text{ A m}^2 \text{ V}^{-2}) E_o^2$. **(c)** Characteristic gas velocity u as a function of field strength for the NaOH doped flame; positive (\bullet) and negative (\circ) refer to the sign of the charged species driving the jet. The solid curve is $u = (2.9 \times 10^{-6} \text{ m}^2 \text{ V}^{-1} \text{ s}^{-1}) E_o$.

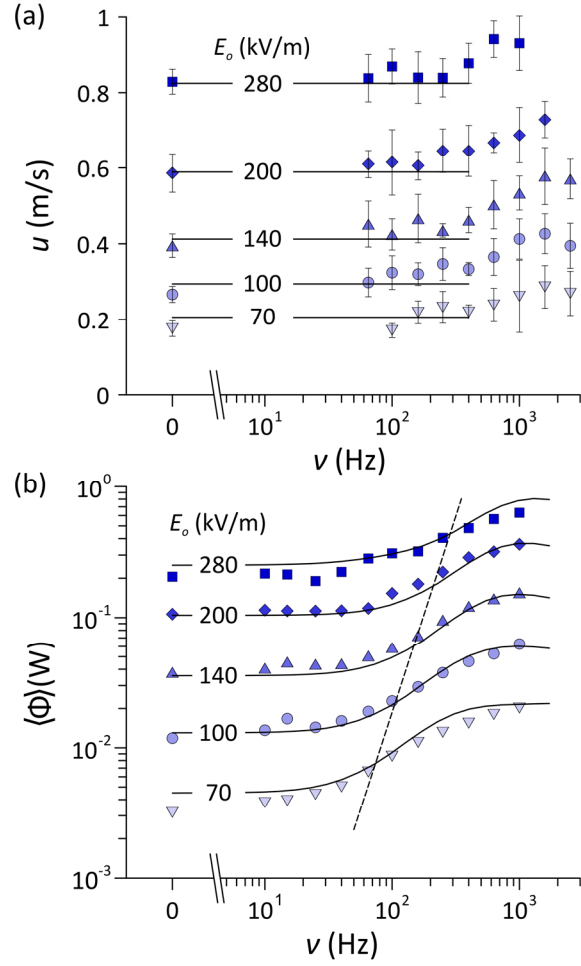


Figure 3. (color online) *Oscillating fields* applied to NaOH-doped, premixed methane flames. **(a)** Characteristic gas velocity u as a function of frequency ν and field strength E_o . The solid lines correspond to $u = (2.9 \times 10^{-6} \text{ m}^2 \text{ V}^{-1} \text{ s}^{-1}) E_o$ as obtained from Figure 2c. **(b)** Average electric dissipation rate Φ as a function of frequency ν and field strength E_o . The solid lines are theoretical predictions of the charge transport model. The dashed line illustrates the transition from the low frequency regime to the high frequency regime as defined by the condition $\delta \sim L$. The parameters used in the model are: electrode spacing, $L = 0.1 \text{ m}$; flame width, $b = 10^{-2} \text{ m}$; flame thickness, $a = 10^{-4} \text{ m}$; mobility, $K = 1.05 \times 10^{-4} \text{ m}^2 \text{ V}^{-1} \text{ s}^{-1}$; recombination rate, $k_r = 1.90 \times 10^{-13} \text{ ions}^{-1} \text{ m}^3 \text{ s}^{-1}$; ionization rate, $k_i = 1.09 \times 10^{20} \text{ ions m}^{-3} \text{ s}^{-1}$; and flame area, $A_f = 3.90 \times 10^{-3} \text{ m}^2$ (see [16] for details).

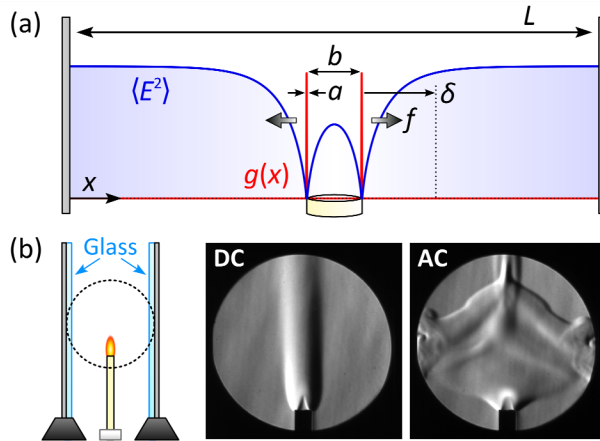


Figure 4. (color online) **(a)** Schematic illustration of the 1D model showing the ionization region $g(x)$ and the time averaged field squared $\langle E^2 \rangle$. **(b)** Electrohydrodynamic response of flame plasmas using glass-insulated electrodes for static ($E_o = 75 \text{ kV/m}$; *left*) and oscillatory ($E_o = 75 \text{ kV}_{\text{RMS}}/\text{m}$, $\nu = 800 \text{ Hz}$; *right*) fields.